

This Page Is Inserted by IFW Operations  
and is not a part of the Official Record

## **BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning documents *will not* correct images,  
please do not report the images to the  
Image Problem Mailbox.**

**PCT**WORLD INTELLECTUAL PROPERTY ORGANIZATION  
International Bureau

## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<b>(51) International Patent Classification <sup>6</sup> :</b> <b>C01B 3/38</b>	<b>A1</b>	<b>(11) International Publication Number:</b> <b>WO 99/35082</b> <b>(43) International Publication Date:</b> 15 July 1999 (15.07.99)
<b>(21) International Application Number:</b> PCT/US99/00629 <b>(22) International Filing Date:</b> 11 January 1999 (11.01.99) <b>(30) Priority Data:</b> 09/005,676 12 January 1998 (12.01.98) US <b>(71) Applicant:</b> REGENTS OF THE UNIVERSITY OF MINNESOTA [US/US]; 100 Church Street Southeast, Minneapolis, MN 55455 (US). <b>(72) Inventors:</b> SCHMIDT, Lanny, D.; 4852 13th Avenue South, Minneapolis, MN 55417 (US). WITT, Paul, M.; Box 8361 Tech Center, South Charleston, WV 25303 (US). <b>(74) Agent:</b> MUETING, Ann, M.; Mueting, Raasch & Gebhardt, P.A., P.O. Box 581415, Minneapolis, MN 55458-1415 (US).	<b>(81) Designated States:</b> AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).  <b>Published</b> <i>With international search report.</i>	
<b>(54) Title:</b> CONTROL OF HYDROGEN AND CARBON MONOXIDE PRODUCED IN PARTIAL OXIDATION PROCESS <b>(57) Abstract</b> <p>A process for enhancing H<sub>2</sub> or CO production in a partial oxidation reaction by feeding H<sub>2</sub>O or CO<sub>2</sub> with the feed hydrocarbon and oxygen over a transition metal monolith catalyst such as unsupported Ni monolith or alternatively contacting the hydrocarbon/oxygen first with a noble metal then with a transition metal with the H<sub>2</sub>O or CO<sub>2</sub> being added before or after the noble metal catalyst. The addition of H<sub>2</sub>O suppresses CO and enhances H<sub>2</sub> production and the addition of CO<sub>2</sub> suppresses H<sub>2</sub> and enhances CO production. Little steam or CO<sub>2</sub> reforming occurs with the addition of up to 32 % H<sub>2</sub>O or CO<sub>2</sub> respectively. Thus, the ratio of H<sub>2</sub>:CO which is about 2 in a conventional partial oxidation is manipulated by the addition of either water or CO<sub>2</sub> to the partial oxidation.</p>		

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece			TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
BY	Belarus	IS	Iceland	MW	Malawi	US	United States of America
CA	Canada	IT	Italy	MX	Mexico	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NB	Niger	VN	Viet Nam
CG	Congo	KE	Kenya	NL	Netherlands	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NO	Norway	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	NZ	New Zealand		
CM	Cameroon			PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakstan	RO	Romania		
CZ	Czech Republic	LC	Saint Lucia	RU	Russian Federation		
DE	Germany	LI	Liechtenstein	SD	Sudan		
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		

## CONTROL OF HYDROGEN AND CARBON MONOXIDE PRODUCED IN PARTIAL OXIDATION PROCESS

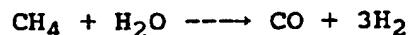
BACKGROUND OF THE INVENTION

## 5 Field of the Invention

The present invention relates to a process and apparatus for production of H<sub>2</sub> or CO by the partial oxidation of hydrocarbons, preferably methane. In particular the partial oxidation is carried out in the presence of water or carbon dioxide under water-gas shift reaction conditions. The invention was made with government support under DOE Grant No. DE-FG02-88ER13878-A02. The government has certain rights in the invention.

## Related Art

15 Catalytic steam reforming of methane is currently the main industrial process to produce synthesis gas (CO and H<sub>2</sub>). The steam reforming reaction may be represented as:



Reforming is highly endothermic, requiring energy input and also requiring contact times on the order of seconds. The resultant high H<sub>2</sub>/CO ratio is also unsuitable for methanol and Fischer-Tropsch synthesis. Therefore additional downstream reactors are usually required to adjust this ratio by water-gas shift reaction at contact time of  $\approx 1$  second as:



Partial oxidation, on the other hand, is an exothermic reaction which can be represented by the reaction of methane with oxygen as follows:



To produce synthesis gas by steam reforming, high temperature heat input is primarily required at two process steps. First, sufficient steam at a high temperature and high pressure must be generated for mixing with the hydrocarbon feedstock and, second, the steam reforming of the steam and hydrocarbon mixture must take place at relatively high temperatures and pressures through a bed of solid catalyst. The equipment needed for these two heat transfers at high temperature and high pressure is

necessarily quite expensive. The equipment for the steam reforming step is also costly because it must be adapted to permit the changing of the solid catalyst when that catalyst is spent or poisoned. Heat sources appropriate for the above two process steps are typically provided by fired heaters at high, continuing utility costs, also with high fluegas  $\text{NO}_x$  production consequential to the high temperatures required in the furnace firebox.

The production of synthesis gas by partial oxidation is considered a desirable alternative to steam reforming since it overcomes some of the problems of steam reforming, see for example PCT publication WO 90/06282 and WO 90/06297. U.S. Pat. No. 4,844,837 to Heck et al discloses a catalytic partial oxidation method for methane using a monolith catalyst with platinum-palladium, palladium-rhodium, or platinum-rhodium coatings. U.S. Pat. No. 4,087,259 to Fujitani et al describes a monolith catalyst with a rhodium coating to perform catalytic partial oxidation on gasoline and heavier petroleum fractions. U.S. Pat. No. 5,648,582 to Schmidt et al discloses the partial oxidation of methane at short residence times using metal deposited on a ceramic monolith.

In these conventional partial oxidations, methane (natural gas) is converted to high purity  $\text{H}_2$  and CO with a mole ratio of  $\text{H}_2:\text{CO} \approx 2.0$ , which is the desired feed ratio for methanol and Fischer-Tropsch plants. However, many other applications require different ratios of  $\text{H}_2:\text{CO}$ . The present synthesis gas shift reactor modifies the prior processes to obtain either high purity  $\text{H}_2$  or CO.

Recent advancements in fuel cell technology have spurred an interest in converting natural gas into hydrogen. Pure hydrogen streams can be produced by steam reforming followed by high temperature shift using an Fe based catalyst, and low temperature shift using a Cu based catalyst. For natural gas to be an effective  $\text{H}_2$  source for fuel cells, the present natural gas conversion technology must be simplified, preferably to a single, highly selective small catalytic reactor. Other applications

include acetic acid production, which requires pure CO feeds. We have discovered that the  $H_2:CO$  product ratio can be altered by the addition of  $CO_2$  or  $H_2O$  through the water-gas shift reaction while the conversion of  $CH_4$  remains constant, indicating negligible reforming is occurring.

#### SUMMARY OF THE INVENTION

Briefly, the present invention is a process for the partial oxidation of hydrocarbons such as methane (natural gas) by contacting a feed containing the hydrocarbon and oxygen and  $H_2O$  or  $CO_2$  through a catalyst zone containing a catalytically effective amount of at least one transition metal monolith catalyst under partial oxidation conditions. A preferred monolith catalyst is a nickel metal monolith. When  $H_2O$  is fed, the product shifts toward the  $H_2$  and when  $CO_2$  is present the product shifts toward  $CO$ , thus the presence of either water or  $CO_2$  provides the means to adjust the  $H_2:CO$  ratio, preferably in the range of more than about 2 to about 6 when water is added and in the range of less than about 2 to about 0.5 when  $CO_2$  is added. It appears that the presence of water or  $CO_2$  in the reaction zone according to the present invention produces a water-gas shift rather than reforming.

In a further embodiment the process comprises a first contacting a feed comprising methane and oxygen feed with or without  $H_2O$  or  $CO_2$  with a noble metal coated onto a monolith. The  $H_2O$  or  $CO_2$  may be fed through the noble metal monolith or between the noble metal monolith and the transition metal monolith.

Because partial oxidation reactions are exothermic, it is not necessary to add external heat to the system other than to obtain ignition of the catalyst.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 shows the conversion of  $CH_4$  and selectivities to  $H_2$  with  $CO_2$  addition over Ni.

Fig. 2 shows the conversion of  $CH_4$  and selectivities to  $H_2$  with  $CO_2$  addition over Rh.

Fig. 3 shows the conversion of  $CH_4$  and selectivities to  $H_2$  with  $CO_2$  addition over Pt.

Fig. 4 shows the conversion of  $\text{CH}_4$  and selectivities to CO with  $\text{H}_2\text{O}$  addition over Ni.

Fig. 5 shows the conversion of  $\text{CH}_4$  and selectivities to CO with  $\text{H}_2\text{O}$  addition over Rh.

5 Fig. 6 shows the conversion of  $\text{CH}_4$  and selectivities to CO with  $\text{H}_2\text{O}$  addition over Pt.

Fig. 7 compares the selectivity to CO in the product with the addition of  $\text{H}_2\text{O}$  over Ni, Rh, and Pt.

10 Fig. 8 compares the ratio of the  $\text{H}_2$  in the product to the  $\text{CH}_4$  in the feed with the addition of  $\text{H}_2\text{O}$  over Ni, Rh, and Pt.

Fig. 9 compares the ratio of  $\text{CO}/\text{CO}_2$  in the product with the addition of  $\text{H}_2\text{O}$  over Ni, Rh and Pt.

15 Fig. 10 compares the conversion of  $\text{CH}_4$  with the addition of  $\text{H}_2\text{O}$  over Ni, Rh, and Pt.

Fig. 11 discloses a single bed catalyst reaction system according to the present invention.

Fig. 12 discloses a multibed catalyst reaction system according to the present invention.

20 Fig. 13 discloses an alternative multibed catalyst reaction system according to the present invention.

#### DETAILED DESCRIPTION

The present catalyst is comprised of a monolith structure either composed of the metal of the catalyst or  
25 coated with the metal of the catalyst. The metals may be in the oxide form during use in the present process. The thickness of the monolith through which the feed gas mixture must pass is from 1 mm to 2 cm. Catalyst contact time ranges from 0.1 to 20 milliseconds when using a  
30 monolith of 50% porosity and 0.2 to 1 cm in depth. Under operating conditions, this corresponds to Gas Hourly Space Velocity (GHSV) of 60,000 to 3,000,000  $\text{hr}^{-1}$ .

Ceramic foam monoliths have been found in the present invention to create the superior mass transfer  
35 characteristics necessary if high space velocities are to be used. The metal monolith may be prepared as metal foam or sintered particles of metal. The solid metal monoliths exhibit superior heat transfer properties but may require

substantial amounts of very expensive metals in some embodiments. Thus, in some applications the metal coated ceramics will be the catalyst of choice. As used herein the term "metal monolith" shall include both the solid metal monoliths and the metal coated ceramic monoliths. The solid metal monoliths may be produced by any method, for example foaming, sintering and fusing.

The reactor is started from ambient temperature through the use of a mixture of light hydrocarbons or ammonia and air preheated to about 200°C and then introduced to the monolith catalyst at an appropriate temperature at which combustion will occur. After combustion has established a monolith catalyst temperature of near 1000°C, preheat and ammonia is stopped. The feed gas mixture of hydrocarbons (methane) and oxygen is then fed to the catalyst zone at a temperature of from 25° to 450°C. Thus, the gas feed mixture of the present invention does not require preheating to near its ignition temperature prior to introduction to the catalyst, thereby avoiding the production of CO<sub>2</sub> and H<sub>2</sub>O and the concurrent reduction of the selectivity for H<sub>2</sub> and CO. With the introduction of water or carbon dioxide to the reaction in accordance with the present invention, the preheat of the feed is adjusted to maintain the established outlet temperature.

The amounts of hydrocarbon, H<sub>2</sub>O, CO<sub>2</sub> and oxygen introduced into the partial oxidation (catalyst zone) are controlled to provide O<sub>2</sub>:C ratios of from about 0.2 to 0.8 and H<sub>2</sub>O or CO<sub>2</sub>:C ratios of about 0.5 to 5. The process is carried out from about atmospheric pressure to about 2000 psig. The amount of water or CO<sub>2</sub> added is preferably up to 45%, more preferably 5 to 35% of the gaseous feed.

Because the hydrocarbon conversion remains constant with or without the H<sub>2</sub>O or CO<sub>2</sub> it appears that little or no reforming is occurring. Thus the present partial oxidation in the presence of H<sub>2</sub>O or CO<sub>2</sub> is characterized as occurring in the substantial absence of reforming. The predominant reaction in the presence of water or CO<sub>2</sub> is characterized as a water-gas shift reaction.



In a preferred embodiment of the present invention, catalytic partial oxidation, an exothermic reaction, takes place in a catalyst monolith having a specified transition metal alone or preceded by a noble metal dispersed to produce a gas which is rich in carbon monoxide and hydrogen. The reaction in the catalytic partial oxidation zone is exothermic and the zone is therefore also referred to as an exothermic catalyst zone. The exothermic, catalytic partial oxidation zone comprises either solid metal monolith and/or a monolithic catalyst carrier or carriers on which transition or transition and noble metal catalyst is dispersed. Such catalyst can effectively catalyze the partial oxidation of, in addition to, gaseous and lighter hydrocarbon liquids such as natural gas or paraffinic naphtha, heavier hydrocarbon liquids such as diesel oil, number 2 fuel oil, and coal derived liquids. As compared to a non-catalytic combustion process such as conventional, non-catalytic partial oxidation, catalytic partial oxidation as described above enables the utilization of lesser amounts of oxygen and lower temperature levels to both oxidize a portion of the feed and crack heavier feedstocks to lighter hydrocarbon fractions while raising the temperature of the reactant mass for subsequent treatment. Generally, at least about half the hydrocarbon feed stock is partially oxidized in the catalytic partial oxidation zone to produce primarily carbon monoxide and hydrogen and heat. Substantially all of the oxygen introduced into the catalytic partial oxidation zone is consumed in the partial oxidation step. The oxygen introduced into the catalytic partial oxidation zone is consumed in the catalytic partial oxidation step. The oxygen may be provided by any suitable "oxygen-containing oxidant gas" which term is used in the claims to include air, air enriched with oxygen, oxygen or oxygen mixed with other gases. The effluent gas from the catalytic partial oxidation zone contains primarily CO, H<sub>2</sub>, H<sub>2</sub>O, N<sub>2</sub>, C<sub>2</sub> to C<sub>4</sub> and other lighter hydrocarbons, including olefins, and, depending upon the sulfur content of the feedstock, H<sub>2</sub>S and

COS. Methane is the preferred feed for  $H_2$  or CO production.

The presence of  $H_2O$  (steam) results in a favorable shift in the product of the  $H_2:CO$  ratio to  $H_2$ , whereas the  
5 presence of  $CO_2$  shifts the ratio in favor of CO.

The combination of features provided by the present invention provides a highly efficient and flexible method of converting various types of hydrocarbonaceous feeds to a hydrogen-rich gas. For example, the combination of  
10 features provided by the process of the present invention provides a highly efficient process of manufacturing a synthesis gas by converting various types of hydrocarbonaceous feeds, including hydrocarbon feeds, to a nitrogen and hydrogen-rich gas suitable for use in ammonia  
15 synthesis. By utilizing the catalytic partial oxidation process as described, a wide variety of hydrocarbonaceous feeds may be efficiently and economically converted into a hydrogen-rich gas.

#### The Monolithic Partial Oxidation Catalysts

20 The partial oxidation catalyst either comprises or is supported on a monolithic carrier, that is, a carrier of the type comprising one or more monolithic bodies having a plurality of finely divided gas flow passages extending therethrough. Such monolithic carrier members are often  
25 referred to as "honeycomb" type carriers and are well known in the art. A preferred form of such carrier is made of a refractory, substantially inert, rigid material which is capable of maintaining its shape and a sufficient degree of mechanical strength at high temperatures, for example, up  
30 to about  $3,373^\circ F.$  ( $1,856^\circ C.$ ). Typically, a material is selected for the support which exhibits a low thermal coefficient of expansion, good thermal shock resistance and, though not always, low thermal conductivity. Two general types of material for construction of such  
35 carriers are known. One is a ceramic-like porous material comprised of one or more metal oxides, for example, alumina, alumina-silica, alumina-silica-titania, mullite, cordierite, zirconia, zirconia-spinal, zirconia-mullite,

silicon carbide, etc. A particularly preferred and commercially available material of construction for operations below about 2,000°F. (1,093°C.) is cordierite, which is an alumina-magnesia-silica material. For applications involving operations above 2,000°F. (1,093°C) an alumina-silica-titania material is preferred. Honeycomb monolithic supports are commercially available in various sizes and configurations. Typically, the monolithic carrier would comprise, e.g., a cordierite member of generally cylindrical configuration (either round or oval in cross section) and having a plurality of parallel gas flow passages or regular polygonal cross section extending therethrough. The gas flow passages are typically sized to provide from about 50 to 1,200, preferably 200 to 600, gas flow channels per square inch of face area.

Various honeycombed (reticulated) ceramic structures are described in the art: U.S. Pat. No. 4,251,239 discloses fluted filter of porous ceramic having increased surface area; U.S. Pat. No. 4,568,595 discloses honeycombed ceramic foams with a surface having a ceramic sintered coating closing off the cells; U.S. Pat. No. 3,900,646 discloses ceramic foam with a nickel coating followed by platinum deposited in a vapor process; U.S. Pat. No. 3,957,685 discloses nickel or palladium coated on a negative image ceramic metal/ceramic or metal foam; U.S. Pat. No. 3,998,758 discloses ceramic foam with nickel, cobalt or copper deposited in two layers with the second layer reinforced with aluminum, magnesium or zinc; U.S. Pat. No. 4,863,712 discloses a negative image honeycombed (reticulated) foam coated with cobalt, nickel or molybdenum coating; U.S. Pat. No. 4,308,233 discloses a reticulated ceramic foam having an activated alumina coating and a noble metal coating useful as an exhaust gas catalyst; U.S. Pat. No. 4,253,302 discloses a foamed ceramic containing platinum/rhodium catalyst for exhaust gas catalyst; and U.S. Pat. No. 4,088,607 discloses a ceramic foam having an active aluminum oxide layer coated by a noble metal containing composition such as zinc oxide, platinum and

palladium.

The foam structure is characterized by the number of pores per linear inch and typical foams are produced with 10 to 100 pores per linear inch. The ceramic supports  
5 employed in the present invention are generally of the type disclosed in U.S. Pat. No. 4,810,685 using the appropriate material for the matrix and are generally referred to in the art and herein as "monoliths".

Generally any organic liquid in which the metal salt is soluble may be used to deposit metals on to monolith  
10 supports. The metals may also be deposited from aqueous solutions using the water soluble salts.

Generally from 0.5 to 20 wt % of the metal will be deposited on the monolith (based on the weight of  
15 monolith).

A suitable high surface area refractory metal oxide support layer may be deposited on the carrier to serve as a support upon which finely dispersed catalytic metal may be distended. As is known in the art, generally, oxides of  
20 one or more of the metals of Groups II, III, and IV of the Periodic Table of Elements having atomic numbers not greater than 40 are satisfactory as the support layer. Preferred high surface area support coatings are alumina, beryllia, zirconia, baria-alumina, magnesia, silica, and  
25 combinations of two or more of the foregoing.

The most preferred support coating is alumina, most preferably a stabilized, high-surface area transition alumina. One or more stabilizers such as rare earth metal oxides and/or alkaline earth metal oxides may be included  
30 in the transition alumina (usually in amounts comprising from 20 to 10 weight percent).

The metal monolith may be prepared as metal foam or sintered particles of metal at high temperature. Monolithic supports may also be made from materials such  
35 as nickel or stainless steel by placing a flat and a corrugated metal sheet, one over the other, and rolling the stacked sheets into a tubular configuration about an axis parallel to the corrugations, to provide a cylindrical-

shaped body having a plurality of fine, parallel gas flow passages extending therethrough.

The transition metals useful in the present invention are selected from the groups consisting of Fe, Os, Co, Rh, Ir, Ni Cu, Pd, Pt and mixtures thereof, with Fe, Co, Ni or Cu forming a preferred grouping, more preferably Ni and more preferably as a solid nickel monolith. Nickel supported on alumina monoliths was not found to be useful in the present process.

The noble metals useful in the present invention are selected from the group consisting of Ru, Rh, Pd, Pt and mixtures thereof preferably Pt or Pd.

For Figs. 1-10 runs were carried out in a quartz tube continuous reactor with 18 mm diameter. Identical  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> monoliths without metal were positioned before and after the catalyst to reduce radiation losses. The catalyst and radiation shields were sealed in the quartz reactor by silica-alumina cloth. The temperatures of the front and back sides of the catalyst were measured with Pt-Pt/Rh thermocouples placed between the catalyst and the radiation shields. Rh and Pt catalysts were ignited with a Bunsen burner at a CH<sub>4</sub>/O<sub>2</sub> ratio of 1.8. The fresh Ni spheres were more difficult to ignite, and therefore NH<sub>3</sub> was added to the feed to lower ignition temperature. After ignition, the reactor was insulated by wrapping it in high temperature insulation.

Rh and Pt catalysts were prepared by impregnating  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> foam monoliths (18 mm diameter by 10 mm long) with concentrated metal salt solutions (rhodium chloride in acetone or chloroplatinic acid in H<sub>2</sub>O) which were added dropwise to the monolith and allowed to dry overnight. The samples were further dried at 390 K for 2 hours and then calcined at 870° K for 2 hours in He and reduced at the same temperature in 10% H<sub>2</sub>/Ar for 7 hrs. However, spheres of sintered Ni activated over a period of 6 hours (at normal reaction conditions) catalyzed an oxidation reaction in which the conversion and selectivities steadily increased. Therefore pure sintered Ni metal spheres (Alfa,

-40 mesh, deposition grade, 99.9%) packed to 1 cm deep were used directly. Similar results were obtained with foamed nickel monolith.

Flow rates of high purity O<sub>2</sub>, N<sub>2</sub>, CO<sub>2</sub> and CH<sub>4</sub> were controlled by mass flow controllers with an accuracy of  $\pm 0.01$  standard liters per minute (slpm). Initial experiments with no CO<sub>2</sub> or H<sub>2</sub>O added to the feed were conducted at 4 slpm, CH<sub>4</sub>/O<sub>2</sub> = 1.8 and 35% dilution, which is optimal fuel/oxygen ratio for syngas production. For all of the CO<sub>2</sub> results presented here, the N<sub>2</sub> was replaced by CO<sub>2</sub> to maintain a constant contact time within the catalyst. The exit temperature of the catalyst was held constant by preheating the feed gases. Runs were repeated where CO<sub>2</sub> was added to a constant flow of CH<sub>4</sub>, O<sub>2</sub> and N<sub>2</sub>. These results are nearly identical and show the same trends as the data presented here and are omitted. For runs in which steam was added to the feed, water was supplied by a syringe pump through a two stage vaporizer and a back pressure regulator to eliminate system pulsing. In all results reported, H<sub>2</sub>O was added to a constant flow of CH<sub>4</sub>, O<sub>2</sub> and N<sub>2</sub>.

Product gases were analyzed by a HP 5890 gas chromatograph with a thermal conductivity detector and integrated by an on-line computer. The detected reaction products were H<sub>2</sub>, CO, CO<sub>2</sub> and H<sub>2</sub>O on all catalysts, and over Pt up to 1% C<sub>2</sub> products were observed. CH<sub>4</sub> conversion and products selectivities were calculated as described previously. For CO<sub>2</sub> addition, the selectivities to CO and CO<sub>2</sub> are not reported (the only carbon containing product that is not a reactant is CO). Similarly H<sub>2</sub> and H<sub>2</sub>O selectivities are not reported for H<sub>2</sub>O addition. In all runs the carbon and hydrogen balances closed with an accuracy better than 97%.

Figs. 1-3 show the conversions of CH<sub>4</sub> and selectivities to H<sub>2</sub> with CO<sub>2</sub> addition on Ni, Rh and Pt catalysts. The reaction temperatures on Ni, Rh and Pt catalysts were held constant with CO<sub>2</sub> addition, 1240°, 1250° and 1500° K, respectively. The equilibrium predictions of CH<sub>4</sub>

conversion and  $H_2$  selectivities at these temperatures are shown by the dashed lines. Since Pt produces a lower  $H_2/H_2O$  ratio, its temperature is  $\approx 250^\circ C$  hotter than Ni or Rh.

5        The  $CH_4$  conversions were nearly constant up to 30%  $CO_2$  addition on all three catalysts, but significantly lower than the equilibrium  $CH_4$  conversions which is nearly 100%. These results imply that little  $CO_2$  reforming of  $CH_4$  occurs at contact times of  $\approx 5$  ms and  $\approx 1300^\circ K$ . Fig 1 also shows  
10       that the conversion of  $CH_4$  is higher on Rh (80%) than on Ni (72%) with Pt (54%) being much less active.

      The addition of  $CO_2$  decreases the selectivity to  $H_2$  over all three catalysts, but to very different amounts. With 24%  $CO_2$  addition on Ni, the  $H_2$  selectivity decreases from  
15       80% to 55%, on Rh it decreases from 84% to 67%, and on Pt it decreases from 59% to 41%. The  $H_2$  selectivities are roughly parallel to, but lower than, the calculated equilibrium  $H_2$  selectivities. These results indicate that  $CO_2$  reacts with  $H_2$  in the reverse water-gas shift reaction  
20       to a greater extent on Ni and least on Pt.

#### Addition of $H_2O$

      The results of  $H_2O$  addition with a constant flow of  $CH_4$ ,  $O_2$ , and  $N_2$  over Ni, Rh or Pt are shown in Figs. 4-6. In these runs, the temperature was kept constant at the  
25       adiabatic temperature in the absence of  $H_2O$  by preheating the gas stream. Because of preheat limitations, maintaining a constant temperature on the Pt catalyst at greater than 12 Vol%  $H_2O$  feed was difficult and therefore is not reported.

30       Figs. 4-6 show that the  $CH_4$  conversions were nearly constant over the entire range of  $H_2O$  addition on all three catalysts, indicating that negligible steam reforming of  $CH_4$  is occurring under these conditions.

      As  $H_2O$  is added to the feed the selectivity to CO  
35       decreases on Ni and Rh but remains essentially constant over Pt. On Ni, the selectivity to CO decreases from 88% to 50% while on Rh the selectivity only drops from 94% to 87%. The  $H_2O$  seems to be reacting with CO by the water-gas

shift reaction over Ni and Rh but not over Pt.

The present results exhibited no catalyst deactivation on unsupported Ni and on supported Pt and Rh for over 100 hours of operation at atmospheric pressure. The present data also show that as the concentration of CO<sub>2</sub> in the feed increases, the conversion of CH<sub>4</sub> remains constant. This clearly shows that CO<sub>2</sub> reforming is not occurring significantly at temperatures near 1300° K, at contact times near 1 ms and in the presence of oxygen.

Although these results may seem contradictory to previous literature, three distinct factors differentiate this work from previous results. First, the present reactor runs adiabatically and autothermally, therefore the reaction temperature is controlled by the catalyst selectivity and the temperatures typically run 250 to 500° hotter than typical CO<sub>2</sub> reforming runs. Second, the contact time over the catalyst in our runs is approximately 1 ms, corresponding to a gas hourly space velocity GHSV of  $-1 \times 10^5 \text{ h}^{-1}$ , which is approximately a factor of 10 higher than most previous CO<sub>2</sub> reforming work. Finally, the presence of O<sub>2</sub> may inhibit CO<sub>2</sub> reforming reactions. The CH<sub>4</sub> is probably reacting with O<sub>2</sub> very rapidly, and the extremely short contact times prevent the remaining CH<sub>4</sub> from reacting with CO<sub>2</sub>.

Similar results have been reported by Choudhary et al., Catal. Lett. 32 (1995) 391-396 over NiO-CaO catalyst at space velocities of up to  $5 \times 10^5 \text{ cm}^3 \text{ g}^{-1} \text{ h}^{-1}$  and temperatures up to 900°C. For CO<sub>2</sub> reforming in the absence of O<sub>2</sub>, the NiO-CaO catalyst coked very rapidly, but when O<sub>2</sub> is added to the feed, the catalyst showed no deactivation due to coke formation. They used their results to show that the addition of O<sub>2</sub> overcomes the endothermic limitations of CO<sub>2</sub> reforming by initially combusting part of the CH<sub>4</sub>. The energy released by combustion can then be immediately used to drive the reforming reactions. They confirmed this by calculating the ratio of CO<sub>2</sub> reforming to oxidative conversion of CH<sub>4</sub> based on the chemistry being controlled by three reactions: 1) partial oxidation of CH<sub>4</sub> with O<sub>2</sub> to



syngas, 2) complete combustion of  $\text{CH}_4$ , 3) and  $\text{CO}_2$  reforming of  $\text{CH}_4$ .

Although, this may be a valid explanation of the product distribution in these experiments, it is believed that present results are better described by the direct oxidation of  $\text{CH}_4$  to syngas followed by water-gas shift. Figs. 1-3 show that as  $\text{CO}_2$  is added to the feed, the conversion of  $\text{CH}_4$  does not change when the outlet temperature is held constant, for example by preheating the feed, indicating that  $\text{CO}_2$  reforming of  $\text{CH}_4$  is probably not active at these contact times and temperatures. However, as  $\text{CO}_2$  is added the selectivity to  $\text{H}_2$  decreases over all three metals. This implies that  $\text{CO}_2$  is reacting with  $\text{H}_2$  in the reverse water-gas shift.

The present results show that the water-gas shift reaction is being affected by the addition of  $\text{H}_2\text{O}$ , particularly over the Ni monolith.  $\text{H}_2\text{O}$  seems to be reacting with CO in the forward water-gas shift to form  $\text{CO}_2$  and  $\text{H}_2$ . The combination of the  $\text{CO}_2$  and  $\text{H}_2\text{O}$  addition results strongly confirm the activity of the water-gas shift reaction and its reverse at  $>1000^\circ \text{K}$  and 1 ms contact time.

As with  $\text{CO}_2$  reforming, steam reforming seems to be inactive over Ni, Rh or Pt at high temperatures and millisecond contact times. This is probably because the  $\text{CH}_4$  preferentially reacts with  $\text{O}_2$  first, and the remaining  $\text{CH}_4$  does not react with the  $\text{H}_2\text{O}$  at these extremely short contact times. This is expected from the relatively low sticking coefficients of  $\text{CO}_2$  and  $\text{H}_2\text{O}$  compared to  $\text{O}_2$ .

The present results show that addition of  $\text{CO}_2$  or  $\text{H}_2\text{O}$  to the feed stream affects the selectivity to  $\text{H}_2$  and CO but leaves the conversion of  $\text{CH}_4$  unaffected. The short contact times, 10 to 10 ms, do not allow significant  $\text{CO}_2$  or steam reforming on any of the three metals, and the dominant reaction is the direct oxidation of  $\text{CH}_4$  to CO and  $\text{H}_2$ .

Since the  $\text{H}_2$  selectivity decreases with the addition of  $\text{CO}_2$  (or CO selectivity decreases with the addition of  $\text{H}_2\text{O}$ ), the water-gas shift reaction or its reverse must be active

at present reaction temperatures and contact times. Therefore, it is believed that the direct partial oxidation of  $\text{CH}_4$  to syngas followed by the water-gas shift reaction are the dominant reactions in the present invention.

Figs. 1-6 show that at contact times near 1 ms, the direct partial oxidation of methane to syngas appears to be followed by water-gas shift or its reverse. Because the water-gas shift reaction is active at 1300° K and 1 ms, the product selectivities can be tuned from high CO to high  $\text{H}_2$  content by introducing  $\text{CO}_2$  or  $\text{H}_2\text{O}$  respectively into the feed stream.

The negligible steam or  $\text{CO}_2$  reforming occurs in the presence of  $\text{O}_2$  over unsupported Ni and  $\alpha\text{-Al}_2\text{O}_3$  supported Rh and Pt catalysts at contact times of 1-10 ms and 1300 K. However, the water-gas shift reaction and the reverse shift reaction are active over Ni and Rh, with Pt being less active. Over Ni, the  $\text{CO}/\text{CO}_2$  ratio decreases to 1 at 30%  $\text{H}_2\text{O}$  addition, which translates to a  $\text{H}_2/\text{CO}$  ratio of 5. This demonstrates the addition of  $\text{H}_2\text{O}$  or  $\text{CO}_2$  can be used to manipulate the ratio of  $\text{H}_2/\text{CO}$  in the product stream.

In Fig. 11 an apparatus with a single transition metal catalyst is illustrated. Hydrocarbon/ $\text{O}_2$  flow 8 is in the direction of the arrow into tubular reactor 10.  $\text{H}_2\text{O}$  (as steam) or  $\text{CO}_2$  enters via line 12 into a bead packing 22. The tubular reactor 10 is wrapped with heating tape and the catalyst 14 is sandwiched between two heat shields 16 and insulated by 18.

In Fig. 12 an apparatus with a multi-catalyst zone is shown in tubular reactor 100. Hydrocarbon/ $\text{O}_2$  feed enters 108 in the direction of the arrow to flow through the reactor.  $\text{H}_2\text{O}$  (steam) or  $\text{CO}_2$  enter into beads 122 via 112 and the mixture contacts noble metal catalyst 114 then transition metal (preferred group) 115. The two catalyst monoliths are associated with heat shields 116 and insulated by 118. The front portion of the reactor containing the beads is wrapped with heating tape 120.

Fig. 13 is a modification of the apparatus of Fig. 12.

The hydrocarbon/O<sub>2</sub> feed 208 enters the tubular reactor 200 and passes through noble metal monolith catalyst 214 which is sandwiched between heat shields 216. That section is insulated by 218. The reaction has been initiated by  
5 igniting the catalyst 214. The product from this partial oxidation passes into the bead packing 222 where it mixes with H<sub>2</sub>O (steam) or CO<sub>2</sub> entering via 212. The mixture proceeds through transition metal (preferred group) monolith catalyst 215. Heating tape is provided to  
10 maintain the temperature from the exothermic partial oxidation.

It has been found that unsupported metal monoliths such as nickel monolith is advantageous over ceramic supported metals. Because of the high thermal conductivity of Ni,  
15 the monolith is a better thermostat and higher flow rates can be achieved with similar selectivities and conversions. By using unsupported Ni, the possibility of nickel-aluminate formation and therefore a deactivation route is eliminated. These two advantages combined allow for  
20 operation over wider range of inlet conditions.

The multiple catalyst bed design takes advantage of a more selective catalyst for synthesis gas formation. In this design the first bed is a supported noble metal catalyst, preferably Rh. This catalyst is supported by a  
25 reticulated or extruded ceramic structure and the weight loadings of catalyst can range from 0.1% to in excess of 10%. Steam or CO<sub>2</sub> is injected immediately following the first catalyst bed prior to entering the second bed. The second bed requires energy input to maintain reaction.  
30 This catalyst can be a noble metal, transition metal or metal oxide, like Ni, Fe, or Cu.

To initiate reaction, the feed gases are introduced to the reactor at the desired flow rate and composition. Energy is added to the catalyst either electrically or  
35 thermally until the catalyst ignites. After catalyst ignition the energy source is removed, and preheat is the only external energy source required to maintain reaction temperatures between 800° and 1000°C. For the multi-bed

reactor, the second and beyond stages may need to be maintained at temperature either by external heating or from the energy released in the first stage.

5 Gas hourly space velocities  $\cdot 10^5 \text{h}^{-1}$  have been used for the process. Inlet compositions of fuel and oxygen were taken from literature sources for the optimal production of synthesis gas. Natural gas was simulated by  $\text{CH}_4$ , the dominant component of natural gas. The inlet compositions ranged from 64% fuel, 36% oxidant to 35% fuel, 20% oxidant  
10 and 45%  $\text{H}_2\text{O}$  or  $\text{CO}_2$ .

The introduction of  $\text{H}_2\text{O}$  into the feed stream results in a decrease in the  $\text{CO}/\text{CO}_2$  ratio. With no  $\text{H}_2\text{O}$  the  $\text{CO}:\text{CO}_2$  ratio is 8:1, but with 40%  $\text{H}_2\text{O}$  feed the ratio is reduced to 1.3:1 when using an unsupported bed of nickel. Adding  $\text{CO}_2$   
15 instead of  $\text{H}_2\text{O}$  results in a decrease in the  $\text{H}_2:\text{H}_2\text{O}$  ratio from 9:1 to 1:1 again over a nickel catalyst. Similar results have been demonstrated over Rh and Pt catalysts.

The invention claimed is:

1. A process for the partial oxidation of hydrocarbons by feeding a stream containing hydrocarbon, oxygen and H<sub>2</sub>O or CO<sub>2</sub> through a catalyst zone containing a catalytically effective amount of at least one transition metal monolith catalyst under partial oxidation conditions wherein said transition metal is selected from the group consisting of Fe, Ru, Os, Co, Rh, Ir, Ni, Cu, Pd, and Pt.
2. The process according to claim 1 wherein the transition metal is Ni or Rh.
3. The process according to claim 1 wherein said catalyst comprises a nickel metal monolith.
4. The process according to claim 1 wherein said catalyst zone contains one transition metal catalyst.
5. The process according to claim 4 wherein the transition metal is Ni or Rh.
6. The process according to claim 1 wherein H<sub>2</sub>O is fed with said hydrocarbon and oxygen.
7. The process according to claim 1 wherein CO<sub>2</sub> is fed with said hydrocarbon and oxygen.
8. The process according to claim 1 wherein at least said hydrocarbon and said oxygen are contacted with a noble metal monolith catalyst under partial oxidation conditions prior to contacting said transition metal monolith catalyst wherein said noble metal is selected from the group consisting of Ru, Rh, Pd, Ir, and Pt.
9. The process according to claim 8 wherein H<sub>2</sub>O is fed with said hydrocarbon and oxygen to contact said noble metal catalyst.
10. The process according to claim 8 wherein CO<sub>2</sub> is fed with said hydrocarbon and oxygen to contact said noble metal catalyst.
11. The process according to claim 8 wherein said H<sub>2</sub>O is fed to said stream after said noble metal monolith catalyst and prior to said transition metal monolith catalyst.
12. The process according to claim 8 wherein said CO<sub>2</sub> is fed to said stream after said noble metal monolith

catalyst and prior to said transition metal monolith catalyst.

13. The process according to claim 1, 4, 6, 7, 8, 9, 10, 11, or 12, wherein said transition metal is selected from the group consisting of Fe, Ru, Os, Co, Rh, Ir, Ni, and Cu.

14. The process according to claim 13 wherein said transition metal is Fe, Cu, or Ni.

15. The process according to claim 14 wherein said transition metal is Cu.

16. The process according to claim 14 wherein said transition metal is Ni.

17. The process according to claim 8, 9, 10, 11, or 12, wherein said noble metal is selected from the group consisting of Pd and Pt.

18. The process according to claim 17 wherein said noble metal is Pt.

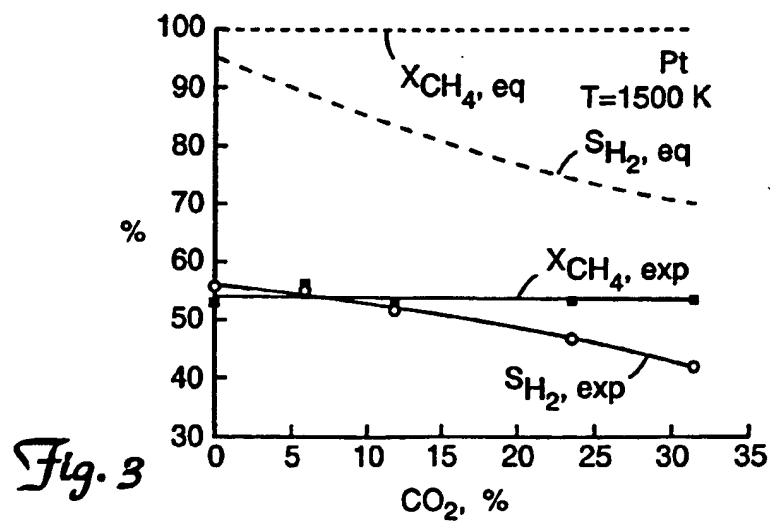
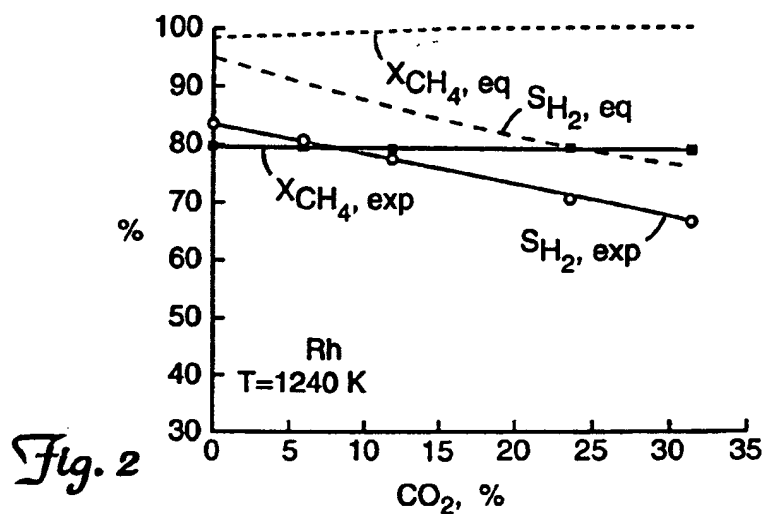
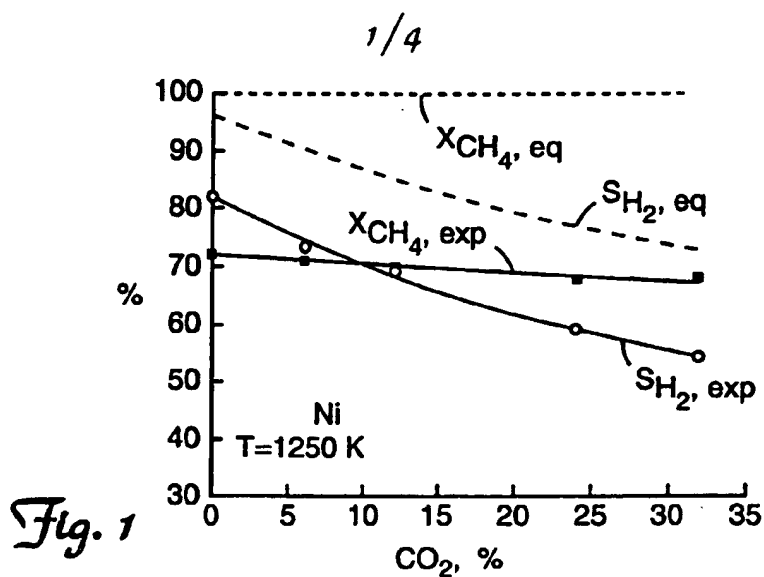
19. The process according to claim 17 wherein said noble metal is Pd.

20. The process according to claim 3 wherein said nickel monolith comprises a foam.

21. The process according to claim 3 wherein said nickel monolith comprises sintered nickel particles.

22. The process according to claim 1 wherein the feed gas to the reaction is preheated to a temperature in the range of 25-450°C.

23. The process according to claim 22 wherein the pressure of the process is in the range of atmospheric to 2000 psig.



2/4

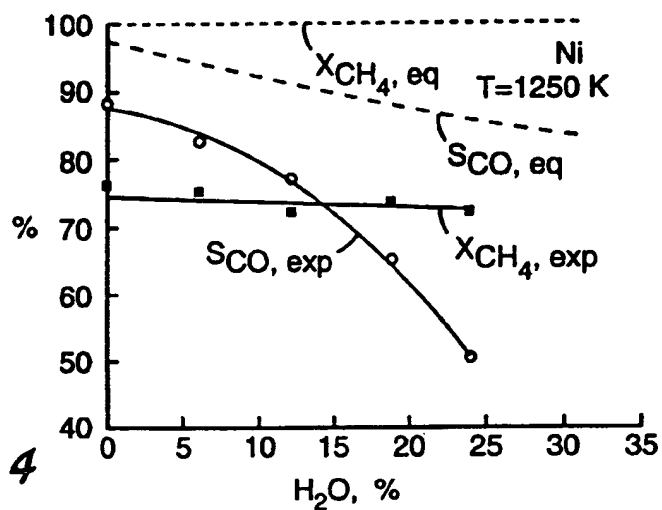


Fig. 4

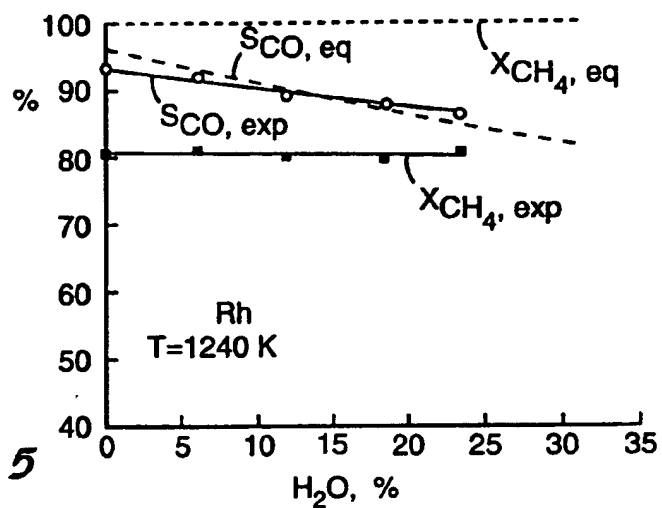


Fig. 5

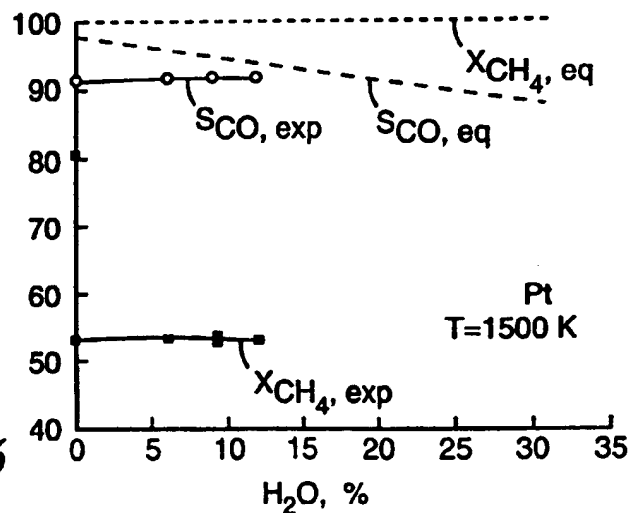
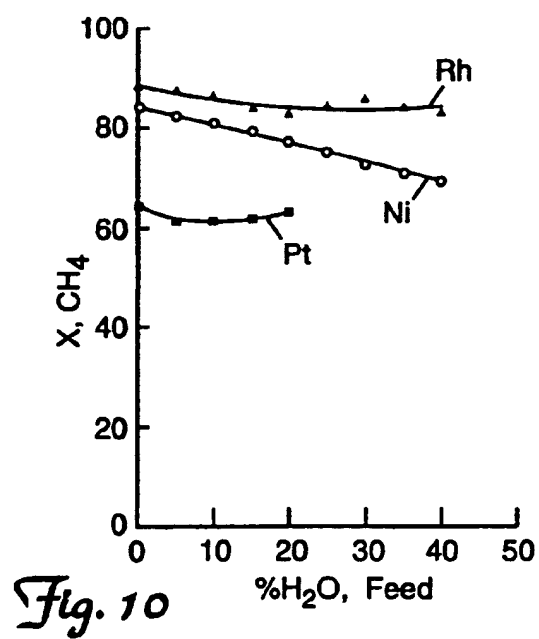
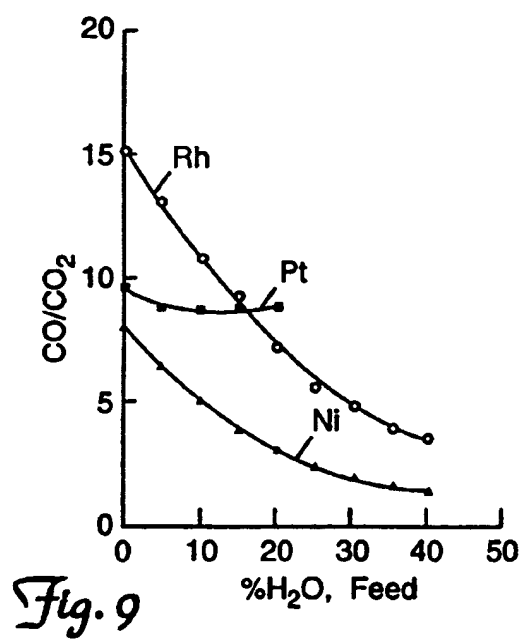
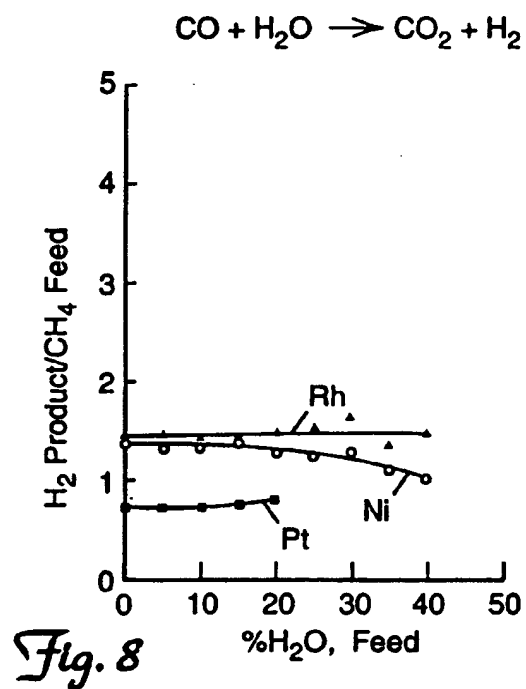
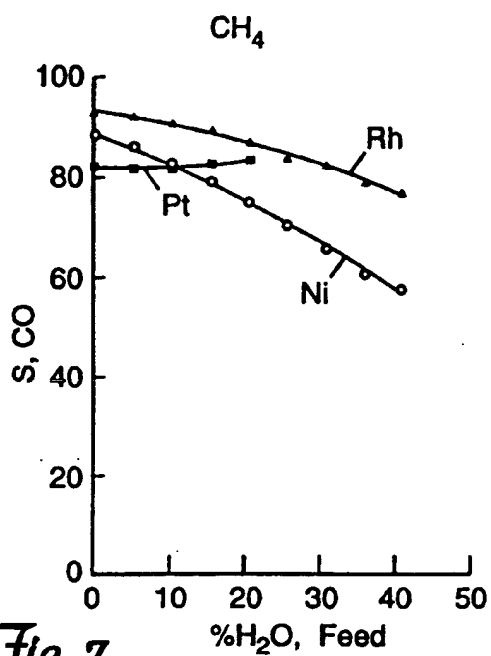


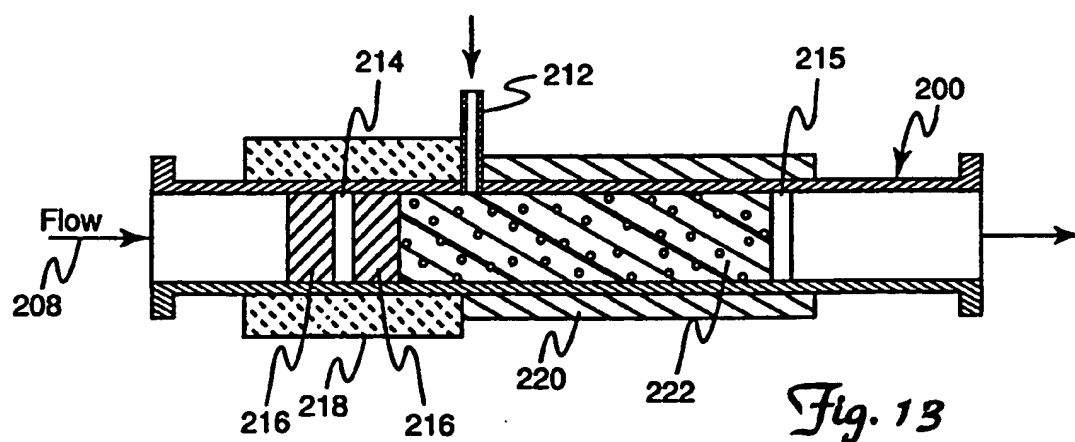
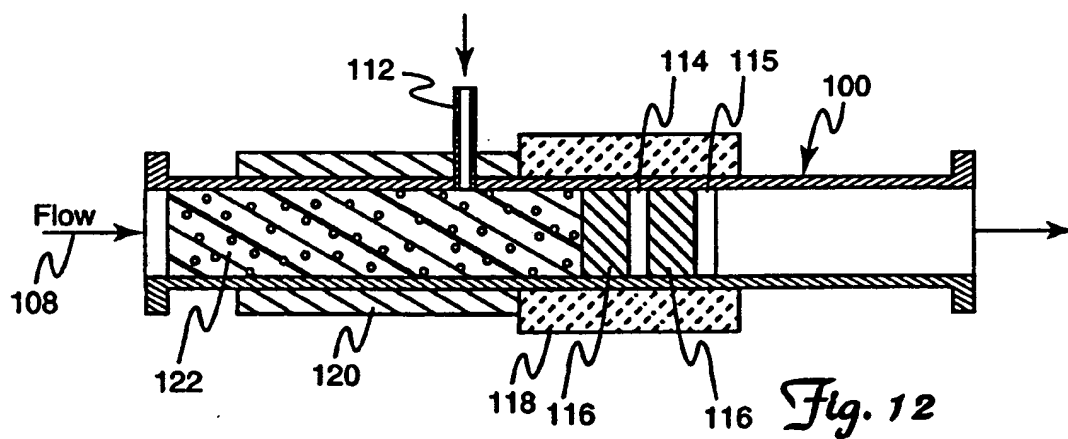
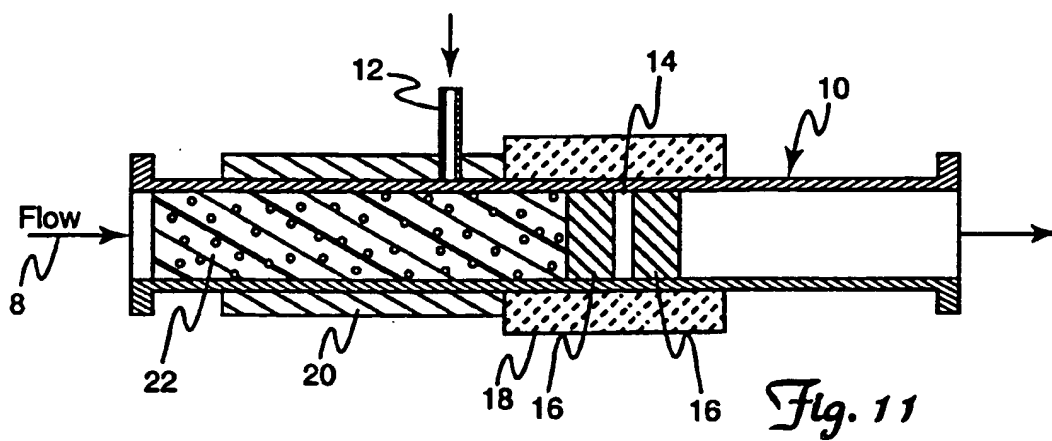
Fig. 6



3/4



4/4



# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 99/00629

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 6 C01B3/38

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 C01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	GB 2 274 284 A (SNAM PROGETTI) 20 July 1994 see page 7, line 16 - page 11, line 10 ---	1-10, 12, 13, 16-23
X	EP 0 645 344 A (SHELL INT RESEARCH) 29 March 1995  see page 3, line 17 - page 4, line 58 ---	1-7, 13, 14, 16, 22, 23
X	HOCHMUTH J K: "CATALYTIC PARTIAL OXIDATION OF METHANE OVER A MONOLITH SUPPORTED CATALYST" APPLIED CATALYSIS B: ENVIRONMENTAL, vol. 1, 1992, pages 89-100, XP000431663 see the whole document --- -/--	1, 4, 6

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
- "8" document member of the same patent family

Date of the actual completion of the international search

14 April 1999

Date of mailing of the international search report

27/04/1999

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2260 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Van der Poel, W

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 99/00629

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>P. M. TORNIAINEN ET AL.: "Comparison of monolith-supported metals for the direct oxidation of methane to syngas"</p> <p>JOURNAL OF CATALYSIS, vol. 146, 1994, pages 1-10, XP000770089 USA see page 6: effect of steam</p>	<p>1-6, 13, 14, 16, 20</p>
X	<p>V. R. CHOUDHARY ET AL.: "Energy efficient methane-to-syngas conversion with low H<sub>2</sub>/CO ratio by simultaneous catalytic reactions of methane with carbon dioxide and oxygen"</p> <p>CATALYSIS LETTERS , vol. 32, 1995, pages 391-396, XP002099617 BASEL; SWITZERLAND cited in the application see the whole document</p>	<p>1-5, 7, 13, 14, 16</p>
X	<p>WO 92 11199 A (ISIS INNOVATION) 9 July 1992 see examples</p>	<p>1-5, 7, 13, 14, 16</p>

# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 99/00629

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
GB 2274284 A	20-07-1994	IT 1256227 B	29-11-1995
		CA 2112519 A	24-06-1994
		CN 1089232 A	13-07-1994
		NO 934736 A	24-06-1994
EP 0645344 A	29-03-1995	AT 168969 T	15-08-1998
		AU 680286 B	24-07-1997
		AU 7414294 A	06-04-1995
		BR 9403803 A	23-05-1995
		CA 2132586 A	24-03-1995
		CN 1104173 A, B	28-06-1995
		DE 69412019 D	03-09-1998
		DE 69412019 T	21-01-1999
		ES 2119065 T	01-10-1998
		JP 7089701 A	04-04-1995
		NO 943512 A	24-03-1995
		NZ 264499 A	21-12-1995
		SG 49079 A	18-05-1998
		ZA 9407334 A	10-05-1995
WO 9211199 A	09-07-1992	AT 169887 T	15-09-1998
		CA 2098605 A, C	25-06-1992
		DE 69130021 D	24-09-1998
		DE 69130021 T	18-03-1999
		EP 0564526 A	13-10-1993
		EP 0780339 A	25-06-1997
		ES 2119808 T	16-10-1998
		JP 2761609 B	04-06-1998
		JP 6503297 T	14-04-1994
		US 5431855 A	11-07-1995
		US 5500149 A	19-03-1996